

10. The linear speed of the thread is the tangential speed of the surface of the spool:

$$v = \Delta x / \Delta t = (3 \text{ m}) / (2 \text{ s}) = 1.5 \text{ m/s.}$$

The angular velocity of the spool is

$$\omega = v/r = (1.5 \text{ m/s}) / (1.5 \times 10^{-2} \text{ m}) = \boxed{100 \text{ rad/s along the axis.}}$$

16. As the wheel comes to rest

$\omega = w_1 t - w_2 t^2 = 0$, so $t = t_1 = w_1 / w_2$. The angle turned during this time interval is

$$\begin{aligned} \theta &= \int \omega dt = \int (w_1 t - w_2 t^2) dt = \frac{1}{2} w_1 t_1^2 - \frac{1}{3} w_2 t_1^3 = \frac{1}{2} w_1 (w_1 / w_2)^2 - \frac{1}{3} w_2 (w_1 / w_2)^3 \\ &= \boxed{w_1^3 / 6w_2^2}. \end{aligned}$$

22. The rotational inertia of the dumbbell about the center is

$$I_1 = m(\frac{1}{2}L)^2 + m(\frac{1}{2}L)^2 = \frac{1}{2}mL^2.$$

The rotational kinetic energy is

$$K_1 = \frac{1}{2} I_1 \omega^2 = \frac{1}{2} [\frac{1}{2} (1.5 \text{ kg})(0.62 \text{ m})^2] [(36 \text{ rev/min})(2\pi \text{ rad/rev}) / (60 \text{ s/min})]^2 = \boxed{2.0 \text{ J}}.$$

The rotational inertia of the dumbbell about the end is

$$I_1 = 0 + mL^2 = mL^2.$$

The rotational kinetic energy is

$$K_1 = \frac{1}{2} I_1 \omega^2 = \frac{1}{2} [(1.5 \text{ kg})(0.62 \text{ m})^2] [(36 \text{ rev/min})(2\pi \text{ rad/rev}) / (60 \text{ s/min})]^2 = \boxed{41 \text{ J}}.$$

28. (a) $\vec{R} = \sum m_i \vec{r}_i / \sum m_i$
 $= [m_1(0 \text{ m}, 0 \text{ m}, 0 \text{ m}) + m_2(0 \text{ m}, 1 \text{ m}, 0 \text{ m})] / (m_1 + m_2)$
 $= \boxed{0 \text{ m}, m_2 / (m_1 + m_2) \text{ m}, 0 \text{ m}}.$

(b) $I_b = \sum m_i \bar{R}_i^2 = m_1 [m_2 / (m_1 + m_2)]^2 + m_2 [1 - [m_2 / (m_1 + m_2)]]^2$
 $= \boxed{m_1 m_2 / (m_1 + m_2) \text{ kg} \cdot \text{m}^2}.$

(c) $I_c = \sum m_i \bar{R}_i^2 = m_1(0) + m_2(0)$
 $= \boxed{0}.$

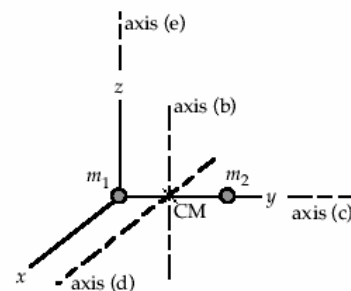
(d) $I_d = \sum m_i \bar{R}_i^2 = m_1 [m_2 / (m_1 + m_2)]^2 + m_2 [1 - [m_2 / (m_1 + m_2)]]^2$
 $= \boxed{m_1 m_2 / (m_1 + m_2) \text{ kg} \cdot \text{m}^2}.$

(e) $I_e = \sum m_i \bar{R}_i^2 = m_1(0)^2 + m_2(1)^2$
 $= \boxed{m_2 \text{ kg} \cdot \text{m}^2}.$

- (f) The parallel-axis theorem for an axis through the origin and along the z-axis is

$$I_e = I_b + Md^2$$

$$= m_1 m_2 / (m_1 + m_2) + (m_1 + m_2) [m_2 / (m_1 + m_2)]^2 = \boxed{m_2 \text{ kg} \cdot \text{m}^2}, \text{ the same as part (e).}$$



31. We choose a thin disk a distance z from the origin with thickness dz

as the element, with mass $dm = \rho \pi r^2 dz$. The density is found from

the mass of the cone: $M = \rho V = \rho (\frac{1}{3}\pi) \tan^2 \alpha H^3$.

The rotational inertia of the disk about the z-axis is $\frac{1}{2} r^2 dm$.

The integral for the rotational inertia of the cone is

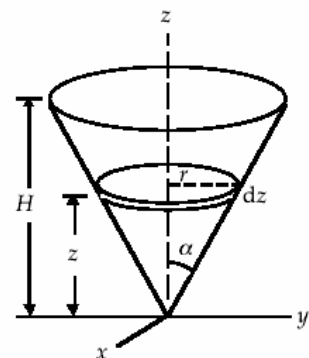
$$I = \int_0^H \frac{1}{2} r^2 \rho \pi r^2 dz.$$

From the diagram we have $r = z \tan \alpha$, so the integral becomes

$$I = \int_0^H \frac{1}{2} \rho \pi z^4 (\tan^4 \alpha) dz = \frac{1}{2} \rho \pi \frac{1}{5} z^5 (\tan^4 \alpha) \Big|_0^H$$

$$= \frac{1}{10} \rho \pi H^5 (\tan^4 \alpha) = \frac{1}{3} \rho \pi (\tan^2 \alpha) H^3 \frac{3}{10} (\tan^2 \alpha) H^2;$$

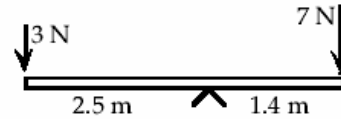
$$I = \frac{3}{10} (\tan^2 \alpha) M H^2.$$



43. (a) We choose the clockwise direction as positive.

$$\tau_{\text{pivot}} = (7 \text{ N})(1.4 \text{ m}) - (3 \text{ N})(2.5 \text{ m}) = \boxed{2.3 \text{ N}\cdot\text{m}}$$

- (b) We see that **changing the 7-N force to 5.4 N** will make the torque zero. An upward force of 8.4 N at the pivot will make the resultant force equal to zero.



48. The uniform distribution of the weight means that the normal force at each wheel is

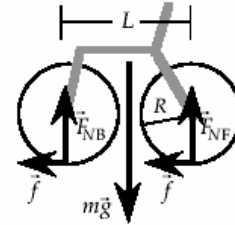
$$F_{\text{NF}} = F_{\text{NB}} = \frac{1}{2}mg = \frac{1}{2}(500 \text{ kg})(9.8 \text{ m/s}^2) = 2.45 \times 10^3 \text{ N}.$$

The maximum friction force at each wheel is

$$f = \mu F_{\text{NF}} = 0.5(2.45 \times 10^3 \text{ N}) = 1.23 \times 10^3 \text{ N}.$$

With the clockwise direction positive, the torque about the center of the front wheel is

$$\begin{aligned} \tau &= F_{\text{NB}}L + 2fR - \frac{1}{2}mgL \\ &= (2.45 \times 10^3 \text{ N})(1.5 \text{ m}) + 2(1.23 \times 10^3 \text{ N})(0.30 \text{ m}) - \frac{1}{2}(500 \text{ kg})(9.8 \text{ m/s}^2)(1.5 \text{ m}) \\ &= \boxed{7.4 \times 10^2 \text{ N}\cdot\text{m}}. \end{aligned}$$



53. The spin angular momentum of Earth is conserved:

$$\frac{2}{5}MR_i^2\omega_i = \frac{2}{5}MR_f^2\omega_f. \text{ Also, } T = 2\pi/\omega. \text{ So}$$

$$T_f/T_i = \omega_i/\omega_f = (R_f/R_i)^2 = [(1 + 0.001\%)R_i/R_i]^2 \approx 1 + 2 \times 10^{-5},$$

and the length of a day would increase by

$$\Delta T \approx (2 \times 10^{-5})T_i = (2 \times 10^{-5})(1 \text{ day})(86400 \text{ s/day}) = \boxed{2 \text{ s}}.$$

57. We write $\Sigma F_x = ma_x$ from the force diagram for the cylinder:

$$Mg \sin \theta - f = Ma;$$

We write $\Sigma \tau = I\alpha$ about the center of mass from the force diagram for the cylinder: $fR = I\alpha$.

For the rolling motion we have $a = R\alpha$.

By successively eliminating α and f , we get

$$a = g \sin \theta / (1 + I/MR^2).$$

For the shell, $I = MR^2$; so $a = \frac{1}{2}g \sin \theta$.

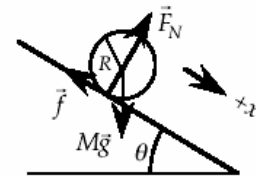
For the linear motion we use

$$x = v_0 t + \frac{1}{2}at^2 = 0 + \frac{1}{2}[\frac{1}{2}(9.8 \text{ m/s}^2) \sin 20^\circ](4 \text{ s})^2 = \boxed{13.4 \text{ m}}.$$

For the solid cylinder, $I = \frac{1}{2}MR^2$; so $a = \frac{2}{3}g \sin \theta$.

For the linear motion we use

$$x = v_0 t + \frac{1}{2}at^2 = 0 + \frac{1}{2}[\frac{2}{3}(9.8 \text{ m/s}^2) \sin 20^\circ](4 \text{ s})^2 = \boxed{17.9 \text{ m}}.$$



61. The rotational inertia of the system about its axis is

$$\begin{aligned} I &= \frac{1}{2}MR^2 + \frac{1}{2}mr^2 \\ &= \frac{1}{2}(0.80 \text{ kg})(0.12 \text{ m})^2 + \frac{1}{2}(0.10 \text{ kg})(0.02 \text{ m})^2 = 5.8 \times 10^{-3} \text{ kg}\cdot\text{m}^2. \end{aligned}$$

For the rolling motion, we write $\Sigma F_x = ma_x$ from the force diagram:

$$(M + m)g \sin \theta - f = (M + m)a;$$

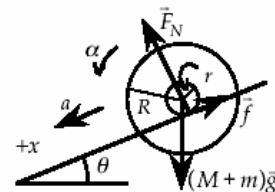
We write $\Sigma \tau = I\alpha$ about the center of mass from the force diagram:

$$fr = I\alpha.$$

For the rolling motion without slipping, we have $a = r\alpha$.

By successively eliminating α and f , we get

$$\begin{aligned} a &= (M + m)gr^2 \sin \theta / [I + (M + m)r^2] \\ &= (0.90 \text{ kg})(9.8 \text{ m/s}^2)(0.02 \text{ m})^2 \sin 5^\circ / [5.8 \times 10^{-3} \text{ kg}\cdot\text{m}^2 + (0.90 \text{ kg})(0.02 \text{ m})^2] = \boxed{0.050 \text{ m/s}^2}. \end{aligned}$$



66. The initial rotational kinetic energy is

$$K_i = \frac{1}{2}I\omega^2 = \frac{1}{2}\left(\frac{1}{2}MR^2\right)\omega^2 = \frac{1}{4}(17 \text{ kg})(0.33 \text{ m})^2[(300 \text{ rev/min})(2\pi \text{ rad/rev})/(60 \text{ s/min})]^2 = \boxed{4.6 \times 10^2 \text{ J}}$$

Because the rotational speed does not change, the increase in the kinetic energy is the kinetic energy of the 0.8-kg mass. The speed of this mass is $R\omega$, so its kinetic energy is

$$K_m = \frac{1}{2}m(R\omega)^2 = \Delta K.$$

The percentage change is

$$\Delta K / K_i = 2m(R\omega)^2 / MR^2\omega^2 = 2m/M = 2(0.8 \text{ kg}) / (17 \text{ kg}) = \boxed{9\%}$$

69. Since the spool will not turn we have $\Sigma\tau = 0$. The force due to the weight of m_1 is m_1g , and its lever arm about the central axis of the spool is R_1 ; so $\tau_1 = m_1gR_1$. Similarly $\tau_2 = -m_2gR_2$. Thus

$$\Sigma\tau = \tau_1 + \tau_2 = m_1gR_1 - m_2gR_2 = 0, \text{ which gives}$$

$$m_2 = \boxed{m_1R_1/R_2}$$

Since the spools does not rotate, its rotational inertia is irrelevant; so making the central cylinder hollow would **not** change the result above.

71. (a) The angular speed of the cylinder is $\omega = v/R$. The angular momentum about the symmetry axis is

$$L = I\omega = MR^2(v/R) = MRv = (3.0 \text{ kg})(0.15 \text{ m})(1.6 \text{ m/s}) = \boxed{0.72 \text{ kg}\cdot\text{m}^2/\text{s}}$$

(b) $K_{\text{rot}} = \frac{1}{2}I\omega^2 = \frac{1}{2}MR^2(v/R)^2 = \frac{1}{2}Mv^2 = \frac{1}{2}(3.0 \text{ kg})(1.6 \text{ m/s})^2 = \boxed{3.8 \text{ J}}$

(c) $K_{\text{total}} = K_{\text{lin}} + K_{\text{rot}} = \frac{1}{2}Mv^2 + \frac{1}{2}Mv^2 = 3.8 \text{ J} + 3.8 \text{ J} = \boxed{7.6 \text{ J}}$

73. The yo-yo will roll to the left with an angular velocity out of the page.

We write $\Sigma F_x = ma_x$ from the force diagram for the yo-yo:

$$F - f_s = Ma;$$

We choose out of the page as positive and write $\Sigma\tau = I\alpha$ about the center of mass from the force diagram for the yo-yo:

$$f_s r - FR = I\alpha = \frac{1}{2}MR^2\alpha.$$

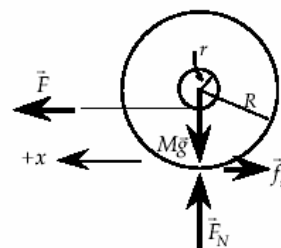
With rolling without slipping, we have $a = R\alpha$.

By successively eliminating α and a , we get

$$F = 3f_s / (1 + 2r/R).$$

Thus the force F will be maximum when the friction force is maximum, which is $f_{s \text{ max}} = \mu F_N = \mu Mg$. Therefore

$$F_{\text{max}} = 3\mu Mg / (1 + 2r/R) = \boxed{3\mu MgR / (R + 2r)}$$



74. (a) When the cylinder is in equilibrium, we write $\Sigma\tau = 0$ about the center of mass from the force diagram:

$$T_0 R = fR = 0, \text{ which gives } T_0 = f.$$

We write $\Sigma F_x = 0$ from the force diagram:

$$f + T_0 - Mg \sin \theta = 0.$$

When we combine the equations, we have $T_0 = \boxed{\frac{1}{2}Mg \sin \theta}$.

- (b) We will assume the acceleration is up the plane.

For the rolling motion, we write $\Sigma F_x = ma_x$:

$$f + T - Mg \sin \theta = Ma.$$

We write $\Sigma\tau = I\alpha$ about the center of mass:

$$TR - fR = I\alpha.$$

For the rolling motion without slipping, we have $a = R\alpha$.

With $I = \frac{1}{2}MR^2$, by successively eliminating α and f , we get

$$a = (2T - Mg \sin \theta) / (M + I/R^2) = \boxed{2(2T - Mg \sin \theta) / 3M}$$

Note that this result holds if the acceleration is down the plane.

The tension and friction force will still be up the plane.

